

# Screening Criterion for Transformer Thermal Impact Assessment

Project 2013-03 (Geomagnetic Disturbance Mitigation)

TPL-007-2 Transmission System Planned Performance for Geomagnetic Disturbance Events

## Summary

Proposed TPL-007-2 includes requirements for entities to perform two types of GMD Vulnerability Assessments to evaluate the potential impacts of GMD events on the Bulk Electric System (BES):

- The benchmark GMD Vulnerability Assessment is based on the benchmark GMD event associated with TPL-007-1 which was approved by the Federal Energy Regulatory Commission (FERC) in Order No. 830 in September 2016. The benchmark GMD event is derived from spatially-averaged geoelectric field values to address potential wide-area effects that could be caused by a severe 1-in-100 year GMD event.<sup>1</sup>
- The supplemental GMD Vulnerability Assessment, based on the supplemental GMD event, is used by entities to evaluate risks that localized peaks in geomagnetic field during a severe GMD event "could potentially affect the reliable operation of the Bulk-Power System".<sup>2</sup> Localized enhancements of geomagnetic field can result in geoelectric field values above the spatially-averaged benchmark in a local area.

The standard requires transformer thermal impact assessments to be performed on BES power transformers with high side, wye-grounded windings with terminal voltage greater than 200 kV. Identified BES transformers must undergo a thermal impact assessment if the maximum effective geomagnetically-induced current (GIC) in the transformer is equal to or greater than:

- 75 A per phase for the benchmark GMD event
- 85 A per phase for the supplemental GMD event

Based on published power transformer measurement data as described below, the respective screening criteria are conservative and, although derived from measurements in single-phase units, are applicable to transformers with all core types (e.g., three-limb, three-phase).

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<sup>1</sup> See *Benchmark Geomagnetic Disturbance Event Description* white paper, May 12, 2016. Filed by NERC in RM15-11 on June 28, 2016.

<sup>2</sup> See Order No. 830 P. 47. On September 22, 2016, FERC directed NERC to develop modifications to the benchmark GMD event, included in TPL-007-1, such that assessments would not be based solely on spatially averaged data. The characteristics of a GMD event for this assessment are in the Supplemental GMD Event Description white paper.

Outside of the differing screening criteria, the only difference between the thermal impact assessment for the benchmark GMD event and the supplemental GMD event is that a different waveform is used, therefore peak metallic hot spot temperatures are slightly different for a given GIC in the transformer.

## Justification for the Benchmark Screening Criterion

Applicable entities are required to carry out a thermal assessment with GIC(t) calculated using the benchmark GMD event geomagnetic field time series or waveform for effective GIC values above a screening threshold. The calculated GIC(t) for every transformer will be different because the length and orientation of transmission circuits connected to each transformer will be different even if the geoelectric field is assumed to be uniform. However, for a given thermal model and maximum effective GIC there are upper and lower bounds for the peak hot spot temperatures. These are shown in **Figure 1** using three available thermal models based on direct temperature measurements.

The results shown in **Figure 1** summarize the peak metallic hot spot temperatures when GIC(t) is calculated using (1), and systematically varying GIC<sub>E</sub> and GIC<sub>N</sub> to account for all possible orientation of circuits connected to a transformer. The transformer GIC (in A/phase) for any value of E<sub>E</sub>(t) and E<sub>N</sub>(t) can be calculated using equation (1) from reference [1].

$$GIC(t) = |E(t)| \cdot \{GIC_E \sin(\varphi(t)) + GIC_N \cos(\varphi(t))\} \quad (1)$$

where

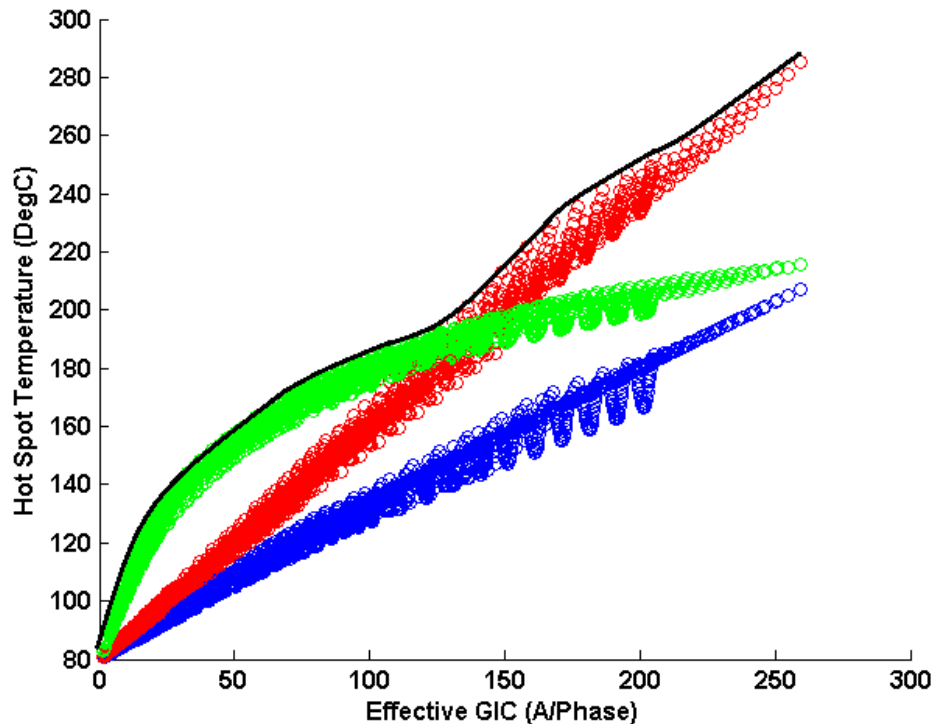
$$|E(t)| = \sqrt{E_N^2(t) + E_E^2(t)} \quad (2)$$

$$\varphi(t) = \tan^{-1}\left(\frac{E_E(t)}{E_N(t)}\right) \quad (3)$$

$$GIC(t) = E_E(t) \cdot GIC_E + E_N(t) \cdot GIC_N \quad (4)$$

GIC<sub>N</sub> is the effective GIC due to a northward geoelectric field of 1 V/km, and GIC<sub>E</sub> is the effective GIC due to an eastward geoelectric field of 1 V/km. The units for GIC<sub>N</sub> and GIC<sub>E</sub> are A/phase per V/km.

It should be emphasized that with the thermal models used and the benchmark GMD event geomagnetic field waveform, peak metallic hot spot temperatures will lie below the envelope shown in black in **Figure 1**. The x-axis in **Figure 1** corresponds to the absolute value of peak GIC(t). Effective maximum GIC for a transformer corresponds to a worst-case geoelectric field orientation, which is network-specific. **Figure 1** represents a possible range, not the specific thermal response for a given effective GIC and orientation.



**Figure 1: Metallic hot spot temperatures calculated using the benchmark GMD event.**

Red: SVC coupling transformer model [2]. Blue: Fingrid model [3]. Green: Autotransformer model [4].

Consequently, with the most conservative thermal models known at this point in time, the peak metallic hot spot temperature obtained with the benchmark GMD event waveform assuming an effective GIC magnitude of 75 A per phase will result in a peak temperature between 160°C and 172°C when the bulk oil temperature is 80°C (full load bulk oil temperature). The upper boundary of 172°C remains well below the metallic hot spot 200°C threshold for short-time emergency loading suggested in IEEE Std C57.91-2011 – Guide for Loading Mineral-Oil-Immersed Transformers and Step-Voltage Regulators [5].

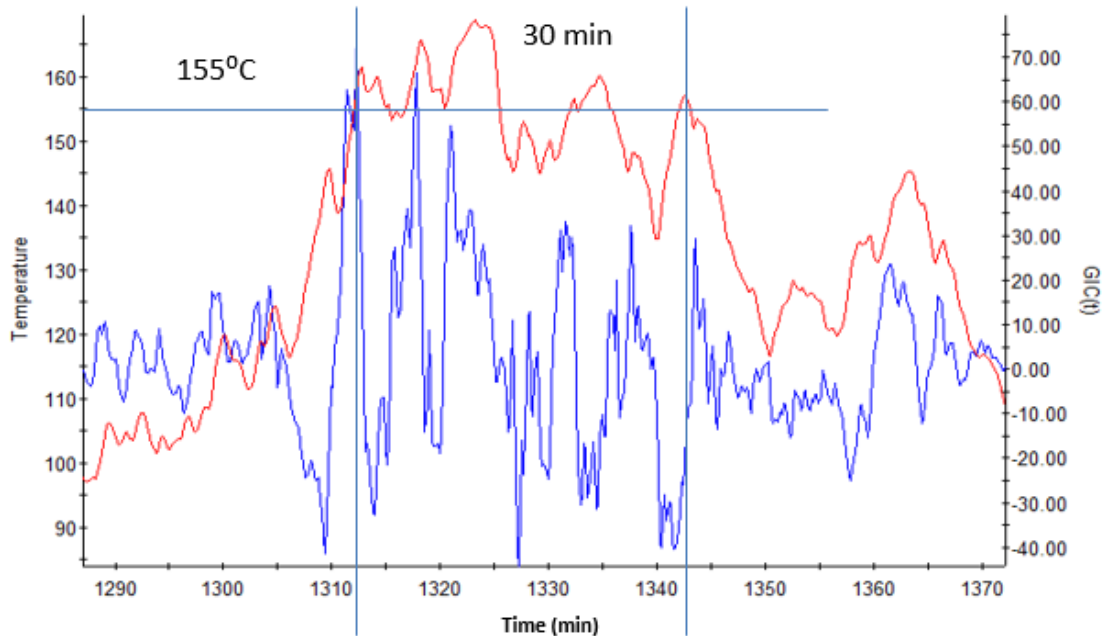
The selection of the 75 A per phase screening threshold is based on the following considerations:

- A thermal assessment, which uses the most conservative thermal models known to date, indicates that a GIC of 75A will not result in peak metallic hot spot temperatures above 172°C. Transformer thermal assessments should not be required by Reliability Standards when results will fall well below IEEE Std C57.91-2011 limits.
- Applicable entities may choose to carry out a thermal assessment when the effective GIC is below 75 A per phase to take into account the age or condition of specific transformers where IEEE Std C57.91- 2011 limits could be assumed to be lower than 200°C. Refer to IEEE Standard C57.163-2015

Guide for Establishing Power Transformer Capability while under Geomagnetic Disturbances for additional information [6].

- The models used to determine the 75 A per phase screening threshold are known to be conservative at higher values of effective GIC, especially the SVC coupling transformer model in [2].
- Thermal models in peer-reviewed technical literature, especially those calculated models without experimental validation, are less conservative than the models used to determine the screening threshold. Therefore, a technically-justified thermal assessment for effective GIC below 75 A per phase using the benchmark GMD event geomagnetic field waveform will always result in a “pass” on the basis of the state of the knowledge at this point in time.
- Based on simulations, the 75 A per phase screening threshold will result in a maximum instantaneous peak hot spot temperature of 172°C. However, IEEE Std C57.91- 2011 limits assume short term emergency operation (typically 30 minutes). As illustrated in **Figure 2**, simulations of the 75 A per phase screening threshold result in 30-minute duration hot spot temperatures of about 155°C. The threshold provides an added measure of conservatism in not taking into account the duration of hot spot temperatures.
- The models used in the determination of the threshold are conservative but technically justified.
- Winding hot spots are not the limiting factor in terms of hot spots due to half-cycle saturation, therefore the screening criterion is focused on metallic part hot spots only.

The 75 A per phase screening threshold was determined using single-phase transformers, but is being applied as a screening criterion for all types of transformer construction. While it is known that some transformer types such as three-limb, three-phase transformers are intrinsically less susceptible to GIC, it is not known by how much, on the basis of experimentally-supported models.



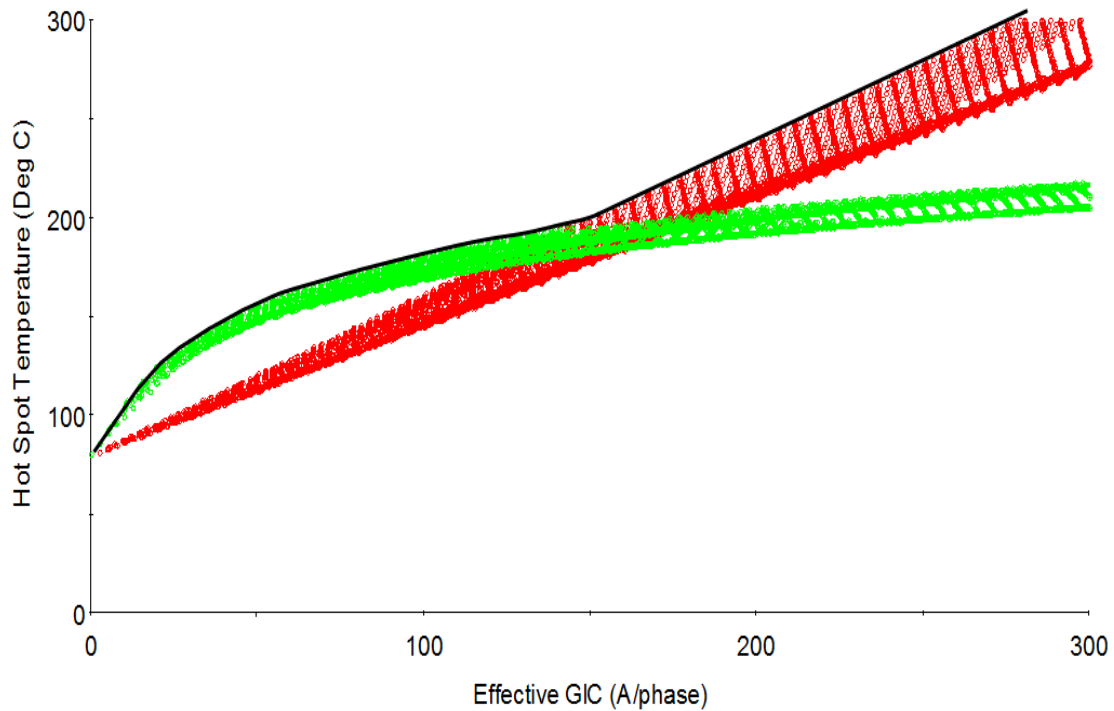
**Figure 2: Metallic hot spot temperatures calculated using the benchmark GMD event.**  
 Red: metallic hot spot temperature. Blue: GIC(t) that produces the maximum hot spot temperature with peak GIC(t) scaled to 75 A/phase.

## Justification for the Supplemental Screening Criterion

As in the case for the benchmark GMD event discussed above, applicable entities are required to carry out thermal assessments on their BES power transformers when the effective GIC values are above a screening threshold. GIC(t) for supplemental thermal assessments is calculated using the supplemental GMD event geomagnetic field time series or waveform.

Using the supplemental GMD event waveform, a thermal analysis was completed for the two transformers that were limiting for the benchmark waveform. The results are shown in **Figure 3**. Peak metallic hot spot temperatures for the supplemental GMD event will lie below the envelope shown by the black line trace in **Figure 3**. Because the supplemental waveform has a sharper peak, the peak metallic hot spot temperatures are slightly lower than those associated with the benchmark waveform. Applying the most conservative thermal models known at this point in time, the peak metallic hot spot temperature obtained with the supplemental GMD event waveform assuming an effective GIC magnitude of 85 A per phase will result in a peak temperature of 172°C when the bulk oil temperature is 80°C (full load bulk oil temperature).<sup>3</sup> Thus, 85 A per phase is the screening level for the supplemental waveform.

<sup>3</sup> The temperature 172°C was selected as the screening criteria for the benchmark waveform as described in the preceding section.

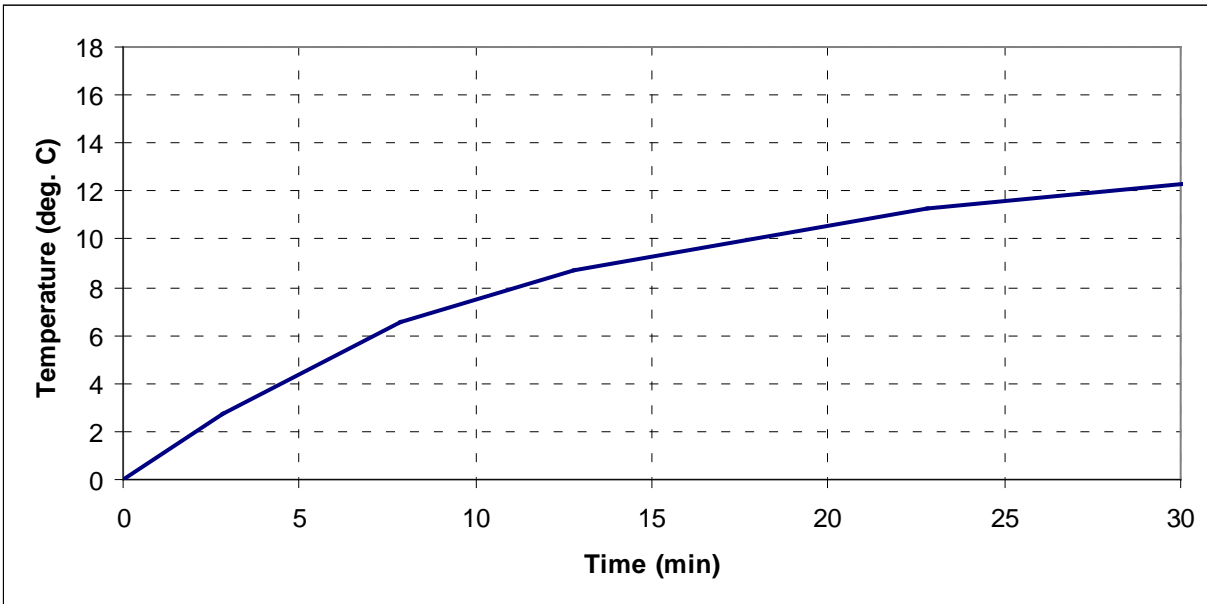


**Figure 3: Metallic hot spot temperatures calculated using the supplemental GMD event.**  
Green: SVC coupling transformer model [2]. Red: Autotransformer model [4]

## Appendix I - Transformer Thermal Models Used in the Development of the Screening Criteria

The envelope used for thermal screening (**Figure 1**) is derived from two thermal models. The first is based on laboratory measurements carried out on 500/16.5 kV 400 MVA single-phase Static Var Compensator (SVC) coupling transformer [2]. Temperature measurements were carried out at relatively small values of GIC (see **Figure I-1**). The asymptotic thermal response for this model is the linear extrapolation of the known measurement values. Although the near-linear behavior of the asymptotic thermal response is consistent with the measurements made on a Fingrid 400 kV 400 MVA five-leg core-type fully-wound transformer [3] (see **Figures I-2 and I-3**), the extrapolation from low values of GIC is very conservative, but reasonable for screening purposes.

The second transformer model is based on a combination of measurements and modeling for a 400 kV 400 MVA single-phase core-type autotransformer [4] (see **Figures I-4 and I-5**). The asymptotic thermal behavior of this transformer shows a “down-turn” at high values of GIC as the tie plate increasingly saturates but relatively high temperatures for lower values of GIC. The hot spot temperatures are higher than for the two other models for GIC less than 125 A per phase.



**Figure I-1: Thermal step response of the tie plate of a 500 kV 400 MVA single-phase SVC coupling transformer to a 5 A per phase dc step.**

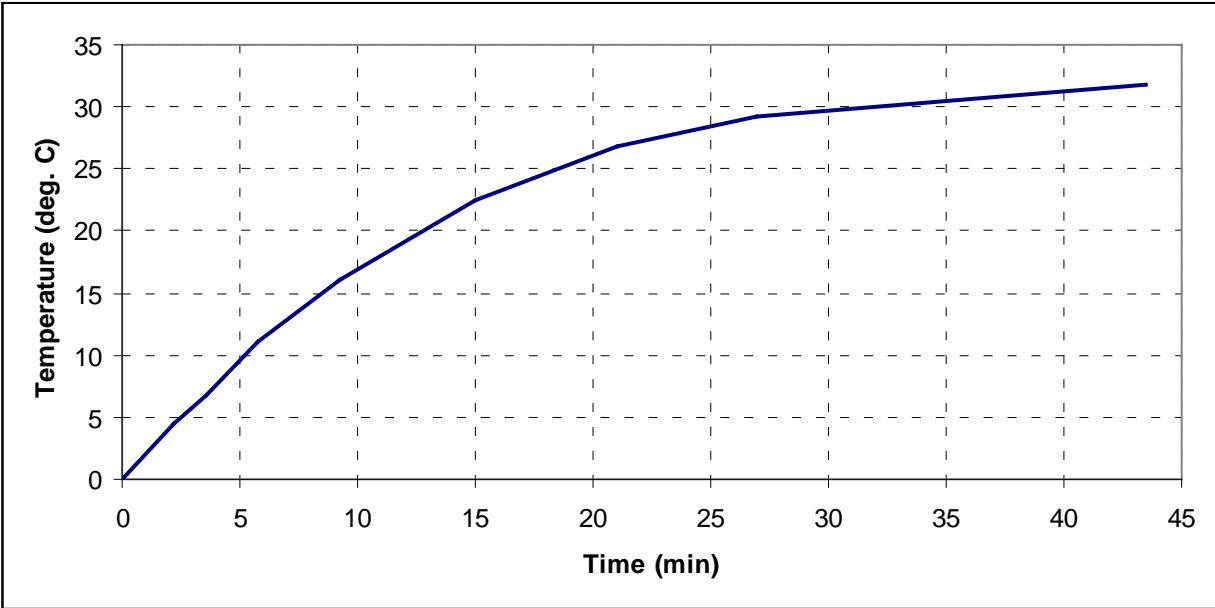


Figure I-2: Step thermal response of the top yoke clamp of a 400 kV 400 MVA five-leg core-type fully-wound transformer to a 16.67 A per phase dc step.

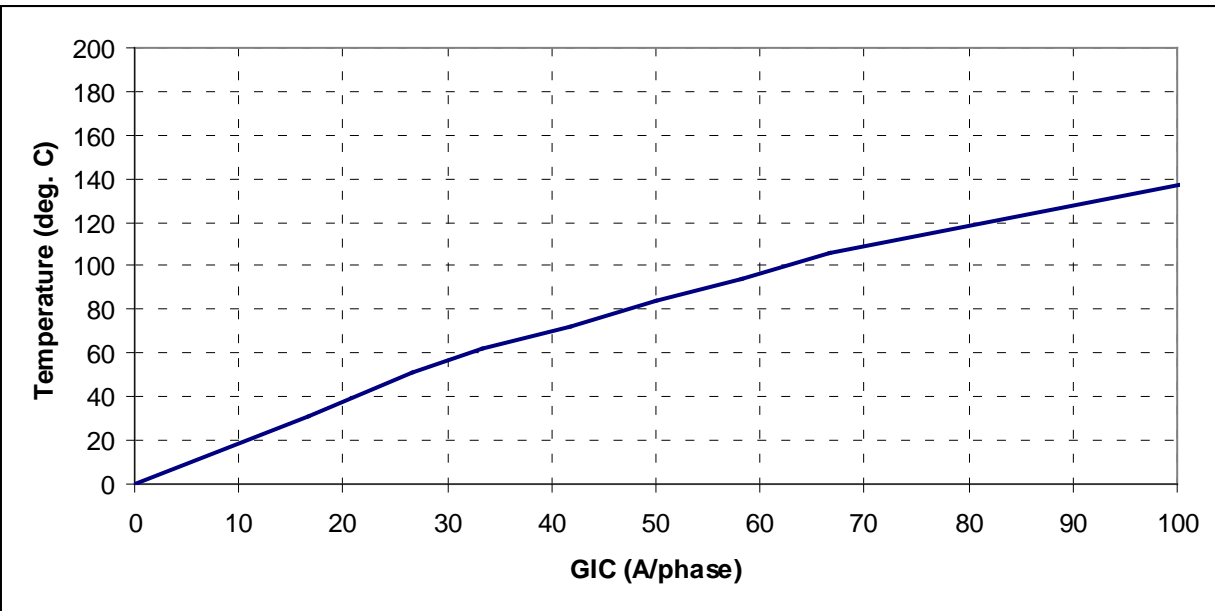


Figure I-3: Asymptotic thermal response of the top yoke clamp of a 400 kV 400 MVA five-leg core-type fully-wound transformer.



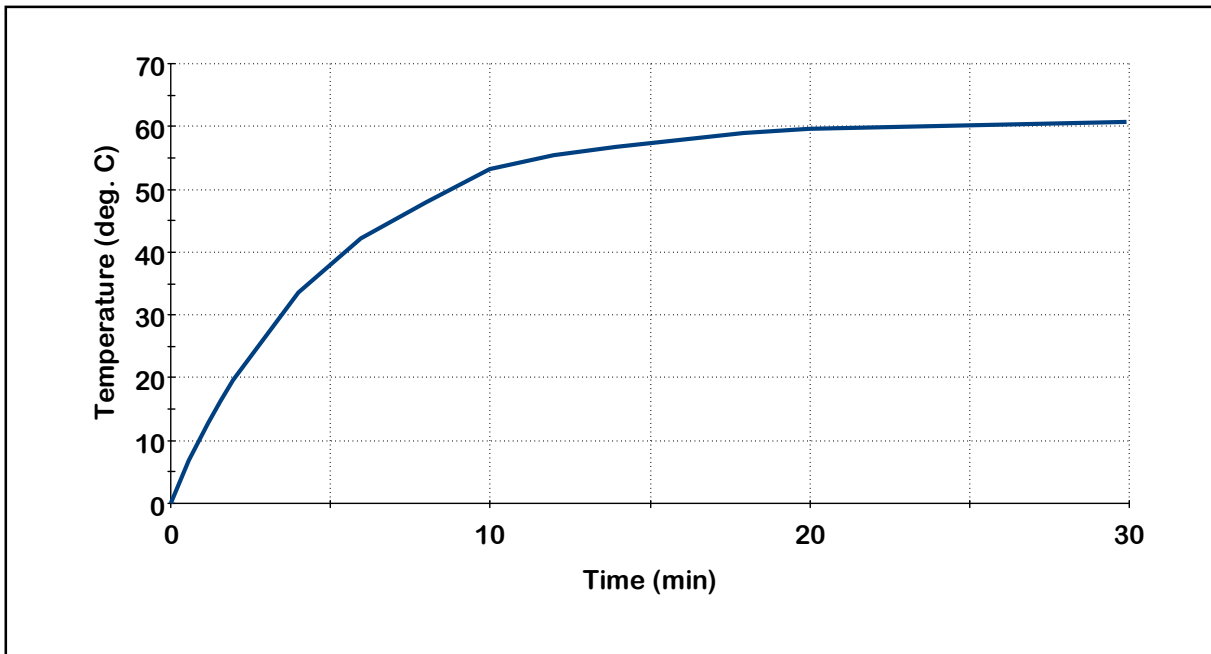


Figure I-4: Step thermal response of the tie plate of a 400 kV 400 MVA single-phase core-type autotransformer to a 10 A per phase dc step.

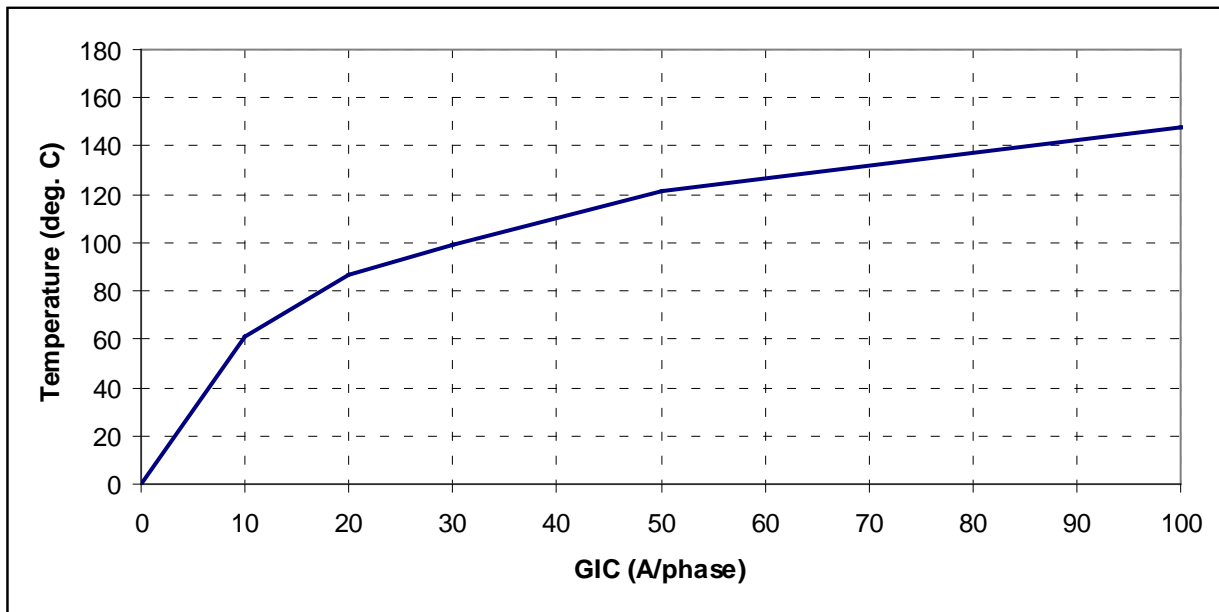


Figure I-5: Asymptotic thermal response of the tie plate of a 400 kV 400 MVA single-phase core-type autotransformer.

The envelope in **Figure 1** can be used as a conservative thermal assessment for effective GIC values of associated with the benchmark waveform (see **Table 1**).

Effective GIC (A/phase)	Metallic hot spot Temperature (°C)	Effective GIC (A/phase)	Metallic hot spot Temperature (°C)
0	80	100	182
10	107	110	186
20	128	120	190
30	139	130	193
40	148	140	204
50	157	150	213
60	169	160	221
70	170	170	230
75	172	180	234
80	175	190	241
90	179	200	247

For instance, if effective GIC is 130 A per phase and oil temperature is assumed to be 80°C, peak hot spot temperature is 193°C. This value is below the 200°C IEEE Std C57.91-2011 threshold for short time emergency loading and this transformer will have passed the thermal assessment. If the full heat run oil temperature is 67°C at maximum ambient temperature, then 150 A per phase of effective GIC translates into a peak hot spot temperature of 200°C and the transformer will have passed. If the limit is lowered to 180°C to account for the condition of the transformer, then this would be an indication to “sharpen the pencil” and perform a detailed assessment. Some methods are described in Reference [1].

The temperature envelope in **Figure 1** corresponds to the values of effective GIC that result in the highest temperature for the benchmark GMD event. Different values of effective GIC could result in lower temperatures using the same model. For instance, the difference in upper and lower bounds of peak temperatures for the SVC coupling transformer model for 150 A per phase is approximately 30°C. In this case, GIC(t) should be generated to calculate the peak temperatures for the actual configuration of the transformer within the system as described in Reference [1]. Alternatively, a more precise thermal assessment could be carried out with a thermal model that more closely represents the thermal behavior of the transformer under consideration.

Similar to the discussion above, the envelope in **Figure 3** can be used as a conservative thermal assessment for effective GIC values of associated with the supplemental waveform (see **Table 2**). Because the supplemental waveform has a sharper peak, the peak metallic hot spot temperatures associated with

the supplemental waveform are slightly lower than those associated with the benchmark waveform. Comparing **Tables 1 and 2** shows the magnitude of this difference.

**Table 2: Upper Bound of Peak Metallic Hot Spot Temperatures Calculated Using the Supplemental GMD Event**

Effective GIC (A/phase)	Metallic hot spot Temperature (°C)	Effective GIC(A/phase)	Metallic hot spot Temperature (°C)
0	80	120	188
10	107	130	191
20	124	140	194
30	137	150	198
40	147	160	203
50	156	170	209
60	161	180	214
70	162	190	229
75	165	200	237
80	169	220	248
85	172	230	253
90	177	250	276
100	181	275	298
110	185	300	316

## References

- [1] Transformer Thermal Impact Assessment white paper. Developed by the Project 2013-03 (Geomagnetic Disturbance) standard drafting team. Available at: <http://www.nerc.com/pa/stand/Pages/TPL0071RI.aspx>
- [2] Marti, L., Rezaei-Zare, A., Narang, A., "Simulation of Transformer Hotspot Heating due to Geomagnetically Induced Currents," *IEEE Transactions on Power Delivery*, vol.28, no.1, pp.320-327, Jan. 2013.
- [3] Lahtinen, Matti. Jarmo Elovaara. "GIC occurrences and GIC test for 400 kV system transformer". *IEEE Transactions on Power Delivery*, Vol. 17, No. 2. April 2002.
- [4] J. Raith, S. Ausserhofer: "GIC Strength verification of Power Transformers in a High Voltage Laboratory", GIC Workshop, Cape Town, April 2014
- [5] "IEEE Guide for Loading Mineral-Oil-Immersed Transformers and Step-Voltage Regulators." IEEE Std C57.91-2011 (Revision of IEEE Std C57.91-1995).
- [6] "IEEE Guide for Establishing Power Transformer Capability while under Geomagnetic Disturbances." IEEE Std C57.163-2015.